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DYNATUNE RIDE & HANDLING "EXPERT" VERSION - RELEASE 8.1

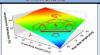
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On each worksheet one can click on the pictures in the header which will redirect to the corresponding web page (left) or the related FAQ support page (right). PASSWORD = dyna4x11989





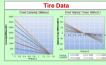
DYNATUNE has been developed in order to provide a convenient MS EXCEL based tool for quick parameter studies based on a eleme ntary car data set. DYNATUNE is entirely based on analytical equations which are commonly available in automotive engineering and for decades have proven their validity. DYNATUNE has been developed to be used especially in the conceptual phase and/or during the final chassis development where it has proved to be also an excellent support for the engineers providing either a quick setup tool allowing theoretical support to their daily business or a useful tracking tool for their data. Every aspect of setting up a car is analyzed in a specific sheet. Main objective for the development of DYNATUNE was providing a robust customer driven development tool in EXCEL with a minimum of data necessary. In RACE & EXPERT Version of DYNATUNE a Laptime Simulator & Test-Tracks have been included with resp. Control panels.

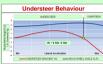
There are 3 main "Sections" in the tool, each with their Specific Application. All Worksheets are related to a Specific Secti on either providing Input Data or presenting detailed Analysis Results.

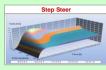


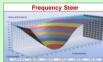


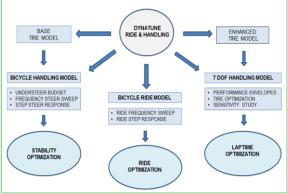


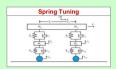






















All frequently used data are being entered in the "MASTER DASHBOARD" sheet. The sheet permits therefore next to simulation control also a quick model overview. From there on the data will be distributed to the various detailed calculation sheets and further specific calculation options can be set. In the various other sheets ADDITIONAL (less commonly modified) data has to be entered.

All relevant vehicle data (Mass, Dimensions, Pay-Load, Aerodynamics etc.) have to be entered in the "VEHICLE DATA" sheet. Inertia Data and Mass Locations are Ride-Height dependent.

In the "CHASSIS DATA" sheet all additional specific SUSPENSION data have to be provided: Basic Kinematic Data, Compliances and Suspension Types. In Version 7.0 and above specific User Guidance Tools are available for Suspension K&C Data.

In the "TIRE DATA" sheet all additional specific TIRE data have to be provided: In Version 7.0 and above specific User Guidance Tools are available for Tire Data. Also an "Enhanced" Tire model is available for more in depth tire data presentation and calculation of tire slip angles.

The "VEHICLE MODEL" sheet represents the core 7 DOF-vehicle model. Based on the requested load condition the 7 DOF-model will calculate all data for the 4 corners and all necessary data will be passed onwards to the other worksheets. Detailed wheel data of all 4 corners are available. From Version 7.0 onwards so called G-G-V Maps can be calculated which plot the vehicle Performance Envelope as function of Ax, Ay and Velocity for traction and braking .

The "SPRING TUNING" sheet provides specific information on typical spring setup parameters of a car. Natural Frequencies, Bounce & Pitch Centers etc.

The "DAMPER TUNING" sheet requires all DAMPER data and allows a typical analysis of damper characteristics like percentage of critical damping and various transient ride transfer functions like Ride Step and Ride Frequency Sweep (Not available in RACE Version).

The "ROLLBAR TUNING" sheet provides all necessary info about basic mechanical balance, based on roll couple distribution, roll center heights and lateral load transfer distribution.

In the "UNDERSTEER" sheet a prediction of the LINEAR range understeer behaviour (UG) is GENERICALLY calculated (based on a bicycle model & the formulas of BUNDORF). Considering spring & rollbar settings (-load transfer) and elementary tire behaviour, understeer gradients are predicted for various g-Levels. Furthermore, if selected in the MASTER DASHBOARD sheet - for a given SPECIFIC lateral acceleration - the UG for one single operating point (considering eventual effects of non-linear bump-stops) can be calculated. From Version 7.0 onwards a full non-linear lateral acceleration sweep can be executed which in combination with the enhanced tire model both provides vehicle and axle slip angles as drivestering wheel langle over the whole lateral acceleration range. Ultimately a unique 4 Dimensional Performance Envelope Graph for Understeer Gradient and Vehicle Side Slip Angle Gradient can be plotted as function of Ax, Ay and Velocity (G-G-V Map).

The "FREQUENCY STEER" sheet calculates the Generic Frequency Steer Response for YAW, SLIP ANGLE and LATERAL ACCELERATION. In addition - if selected in the MASTER DASHBOARD sheet - a specific "Partially Linearized" Frequency Response can be calculated by entering a specific STEERING WHEEL ANGLE (SWA). By doing so, degressive tire vertical & lateral load characteristics will be taken into account for the resulting lateral acceleration. All calculations are based on a bicycle model and linear laplace transformation. Not available in RACE Version

The "STEP STEER" sheet calculates the generic STEP STEER Response for YAW, SLIP ANGLE and LATERAL ACCELERATION. In addition - if selected in the MASTER DASHBOARD sheet - a specific "Partially Linearized" STEP STEER Response can be calculated by entering a specific STEERING WHEEL ANGLE (SWA). By doing so, degressive tire vertical & lateral load characteristics will be taken into account for the resulting lateral acceleration. AIC acculations are based on a bicycle model and linear laplace and standard acceleration. ARGE Version

In the "RESULTS" Sheet one can find for comparison all input and results data for the actual vehicle and a reference vehicle (each in one column) with metrics and plots. Model Data can be im/-exported intoffrom external Excel (*./dsx) sheets.

In the "USER" sheet one can create one's own data. The sheet is unprotected and allows standard EXCEL operations. All Created Data & Graphs can be exported into an external Excel Workbook.

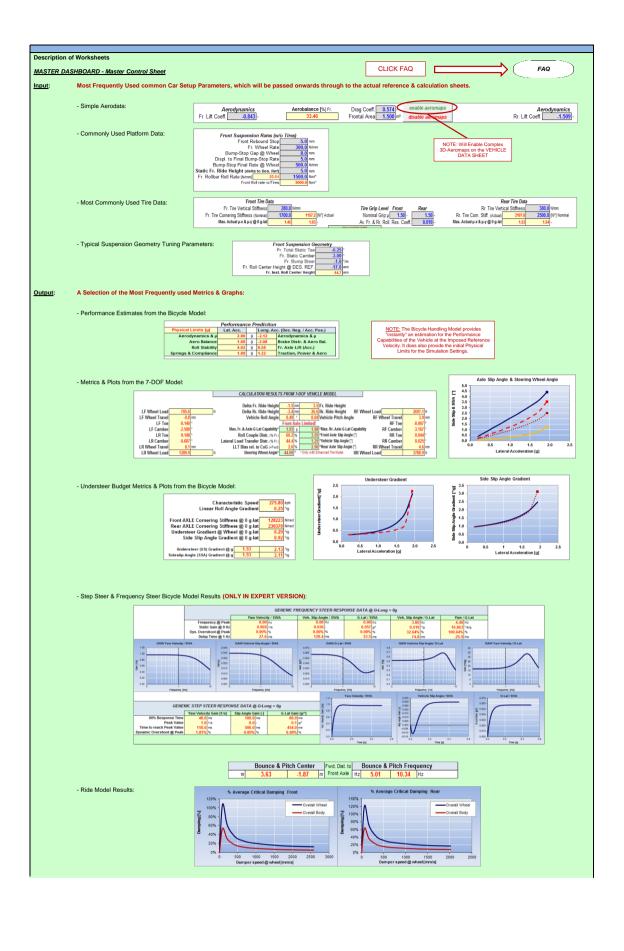
The "CIRCUIT LAYOUT" Sheet does permit the creation of a virtual Test/Race Track/Stage Section. The track MUST consist of at least 4 Straight/Corner sections. The maximum number of corners is 20. All Track-Data is 2D - only. Available are a typical real life High-Speed & Low-Speed Handling Track and a Generic Test Track for quick comparison studies. The ACTUAL Track Layout can be exported/imported into a specific EXCEL file ("Axis) for convenient data transfer.

The "LAPTIME CONTROL" Sheet has become the 2nd heart of DYNATUNE Ride & Handling. In analogy to the "MASTER DASHBOARD" Sheet is here all simulation control concentrated for the Laptime Simulation and related settings.

The "LAP RESULTS" Sheets provides in analogy to the "RESULTS" Sheet a customizable sheet with some example of comparison graphs for a current actual lap and a reference be exported for external postprocessing.

GOTO MASTER

This Workbook requires the activation of iterations in EXCEL options (manual, 50 iterations, 0,001 accuracy)



Running the Simulations:

At the top of the Worksheet one can find a range of buttons for quick navigation through the Workbook and some Data Handling & Import/Export procedures.



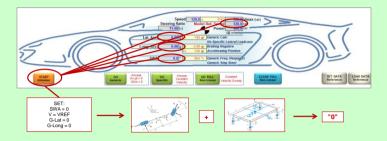
The "START/Initialise" Button will initialise both the Bicycle as the 7-DOF Model to "0" by setting G-Lat = 0, G-Long = 0, Steering Wheel Angle (SWA) = 0 and Model Velocity to Reference Velocity (it will also set some internal iteration parameters to default). After EVERY Setup Change one should run this procedure.

The Bicycle Model is driven by:

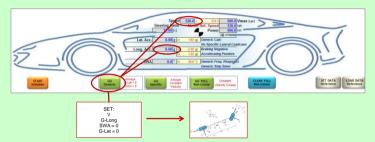
- Speed Longitudinal Acceleration Steering Wheel Angle

The 7-DOF Model is driven by:

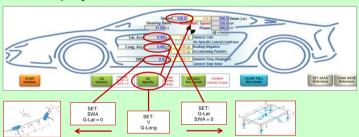
- Speed Longitudinal Acceleration Lateral Acceleration



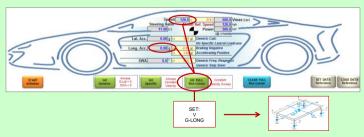
The "GO Generic" Button will run a GENERIC Calculation - primarily addressing the Bicycle Model - and does permit to change only Velocity and Longitudinal Acceleration. The Calculat Procedure will also update all Performance Predictions for the new conditions.



The "GO Specific" Button does run a calculation which will be addressing ONE SPECIFIC Load case for G-Lat, G-Long, SWA & Velocity. However, depending on the Input Values for G-Lat and SWA different models will be used as indicated below. If G-Lat is set to "0" and a SWA is being used, the Bicycle Model will calculate G-Lat out of SWA and calculate the results. If the SWA is set to "0" and a G-Lat Value is used the 7-DOF Model will calculate the corresponding SWA and of course all other Vehicle Data / Metric Data /



The "GO FULL Non-Linear" Button will run a Full-Lateral-Acceleration - sweep from 0 up to the Maximum Possible Lateral Acceleration for the imposed Velocity & Longitudinal Acceleration



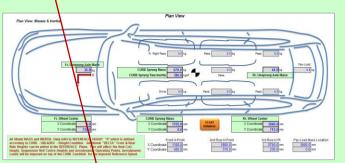
IN RELEASE 8.1 ONE CAN DIFFERENTIATE THE AMOUNT OF TRACTION & REGEN POWER (@ WHEEL) INDEPENDENTLY AND AS SUCH ALLOWING CORRECT SIMULATION OF ICE AND EV POWERTRAIN EFFECTS ON THE DYNAMICS OF THE VEHICLE. THE NEW FEATURE DOES ALSO ALLOW CORRECT IMPLEMENTATION OF DRIVE TORQUE FREEN TORQUE AND ICE OVERRUN CHARACTERISTICS ON THE NEWLY ADDED LIMITED SLIP OFFERENTIALS.

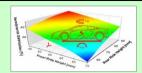
RELEASE 8.1 DOES ALSO ALLOW TO COMBINE REGEN & HYDRAULIC BRAKING IN ORDER TO CORRECTLY REFLECT MODERN BY BRAKE SYSTEMS FULLY CONSIDERING THE PARTICULAR BEHAVIOR OF SUSPENSION ANTI'S.



VEHICLE DATA - Aerodynamics, Dimensions, Masses Input & Other Vehicle Data

Input - Mass Values and Locations of Wheels, Passenger (H-Points) and/or Pay-Load / Ballast Weight:





NOTE: The Vehicle will ALWAYS be kept Symmetrical Left to Right..

All Model MASS and INERTIA Data refer to REFERNCE HEIGHT '0' which is defined according to CURB - UNLADEN - Weight Condition. Additional 'DELTA' Front & Rear Ride Heights can be added to the REFERNCE Plane. This will affect the final CoG-Height. Suspension Roll Centre Heights and Aerodynamic Operating Points. Aerodynamic Losads will be imposed on top of the CURB Condition for the memory fleetings.

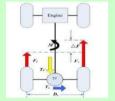
- Brake and Driveline data such as Brake Distribution and Drive Torque Distribution:

RELEASE 8.1 DOES COME WITH QUITE SIGNIFICANT ENHANCEMENTS IN THE POWERTRAIN SECTION. ONE CAN NOW SIMULATE CLASSIC PRE-LOADED LIMITED SLIP DIFFENTIALS AND TURN ON/OFF IDEAL LIR FORCE DISTRIBUTION IN TRACTION OF THE VEHICLE.



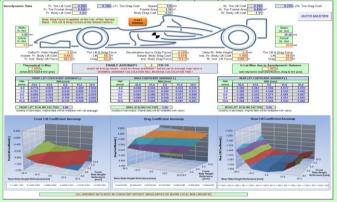
NOTE: One Can Set the Front/Rear Brake Force Distribution to "IDEAL" by entering not a Value but "=OPT_BRAKE_DISTR" in the corresponding Cell.

NOTE: One Can Set the Front/Rear Brake Force Distribution to "IDEAL" by entering not a Value but "=OPT_BRAKE_DISTR" in the corresponding Cell.



Different Left and Right Traction (or Braking Forces) do create a Yaw Moment on the car, which does increase or decrease the amount of Understeer percieved by the driver. When Ideal L/R Braking or Traction Force Distribution is turned off, the simulation will stop when one of the (unloaded) wheels will start slipping. In all Generic and G-Lat = 0 Simulations only the Effects of LSD Preleod will be considerd. The Longitudinal Force Effect on the Yaw Moment of LSD will only be considered when G-Long & G-Lat \Leftrightarrow 0.

- Complex Vehicle Aerodynamic LIFT & DRAG MAPS with their Ride-Height Dependency (Aeromaps):



NOTE: When using Aeromaps one must guarantee that the provided data is consistent and make sure that the ride height data points in the maps are covering the Operating Range of the Vehicle. If NOT the data will be incorrectly fitted or wrongly extrapolated.

Output

- All Relevant Mass and Inertia Data, Weight Distribution & CoG Location:

Total Mass	650.0 kg	Wheel Base	3040.0 mm	CoG Z-Height	233.1 mm	Total Yaw Inertia	605.3 kgm²
Front Mass	275.1 kg	Fr. Track Width	1460.0 mm	CoG X-Position	1753.6 mm	Total Pitch Inertia	534.4 kgm²
Rear Mass	374.9 kg	Rr. Track Width	1430.0 mm	Weight Distribution	42.32 % Front		

- Instantaneous Aerodynamic Lift & Drag Values:

Delta Fr. Ride Height	-1.5 mm Tire Life	& Drag Force	Deceleration due to Drag Forces	-0.129 g	Delta Rr. Ride Height	-3.4 mm	Tire Lift & Drag Force
Instant. Fr. Body Lift Coef. 0.	843 - Lif	69.3 N	Instant. Body Drag Coef.	0.574	Inst. Rr. Body Lift Coef.	-1.509 -	Lift 54.0 N
Fr. Inst. Body Lift Force -84	13.0 N Drag	-62.4 N	Inst. Body Drag Force	-574.5 N	Rr. Inst. Lift Force	-1508.7 N	Drag -63.0 N

REFERENCE RIDE HEIGHT IS DEFINED @ CURB WEIGHT. ONE CAN ADD ON THE MASTERSHEET A "STATIC" RIDEHEIGHT WHICH WILL BE "ON TOP" TO REF. RH. Unsprung Masses are located @ X,Y Wheel Locations and @ Tire Static Loaded Radius Z - Location.

CHASSIS DATA - K&C Suspension Data

- Suspension Type Selection (Independent, Semi-dependent, Solid axle): Input

	Axle Type					
0 = Independent	Front	Rear	U = Understeer O = Oversteer			
1 = Solid Axle	0	0	N = Neutral			
2 = Twist Beam (rear only)	Independent	Independent	N - Neutral			

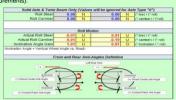


IN RELEASE 8.1 THE STEERING SYSTEM HAS BEEN REFINED WITH ALL NECESSARY PARAMETERS TO CALCULATE MORE ACCURATELY WHEEL STEER ANGLES & STEERING WHEEL TORQUE FEEDBACK CAUSED BY LATERAL FORCES AND LONGITUDINAL FORCES (Torque Steer).

Front Suspension Steering System Data								
Outer Wheel KP Off. Change w/ Wheel Steer Angle [mm/*]	0.0		King Pin Offset (mm)					
Outer Wheel Scr. Rad. Change w/ Wheel Steer Angle [mm/*]	0.0	10.0	Scrub Radius (mm)					
Outer Wheel Trail Change w/ Wheel Steer Angle [mm/*]			Caster Trail (mm)					
Percentage Ackermann	100.0	N						

Steering Parameters will not be automatically imported when using SDM Data Import Procedure but will have to be entered manually.

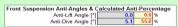




Compliant Data are entered as linear rates. - Roll Center Location & Roll Center Migration Data:



- Anti-Dive and Anti-Squat Angles:

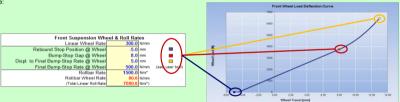


- Special Spring / Rollbar Configurations typically used in Racing Environments (Mono Spring / 3rd Spring Configurations):

✓ COUPLE HEAVE SPRING RATE AND ANTI-ROLLBAR RATE IN ROLL (STANDARD SETTING)

Typically the Heave-Springs do add to the Total Rollirate of the Suspension. However one can create Suspension Spring & Rollibar Linkages which do allow to De-Couple Heave Spring Rate from Anti-Rollibar Rate completely. When De-Coupled, the Heave Springs & Bumpstops will NOT contribute to the Total Rollirate. In such case please START/INTIALIZE the Model new.

- Wheel Load Deflection Curve: Output



Wheel rates are linear. If applicable a NON-LINEAR Bump-Stop can be superimposed.

Bump-Stop is defined by Bump-Stop Gap, Bump-Stop Final Rate & Bump-Stop Displacement to Final Bump-Stop Rate.

See User Tool on Sheet.

- Side-View Swing Arm Locations & Suspension Anti - Percentages (Derived from Anti-Angles, CoG Height, Wheelbase and Brake Force Distribution Percentage)



ALL SUSPENSION DATA REFER TO WHEEL PLANE AND NOT TO COMPONENT DATA

Version 8.0 and above comes with specific knowledge base for K&C Data.

TIRE DATA - Tire Graphs and Tire Database

Input

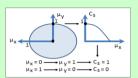
All relevant Tire Parameters

- Reference Load
- Cornering Stiffness
- Aligning Torque Stiffness
- Camber Thrust Rate
- Tire CS/AT/Camber Stiffness Load Dependency
- % Growth of Loaded Radius w/ Speed
- % Longitinal Grip Loss per ° Camber/Inclination Angle
- NEW: % Conering Grip Loss/Gain per kN from Ref. Load

- Tire Model Selection: BASE TIRE MODEL vs. ENHANCED TIRE MODEL

✓ USE ENHANCED TIRE MODEL





Output BASE TIRE:

- Cornering Stiffness Maps:
- Aligning Torque Stiffness Maps:
- Camber Thrust Rate Maps:

Camber Innustrate waps:

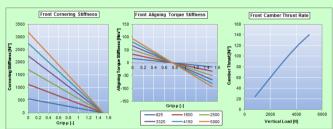
GENERIC LINEAR BASE TIRE MODEL:

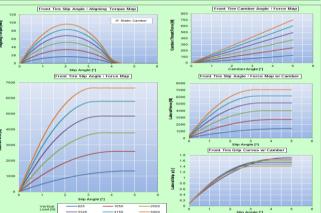
- LINEAR CORNERING STIFFNESS
- LINEAR ALIGNING TOROUG STIFFNESS
- LINEAR CAMBER THRUST RATE
NO TIRE LATERAL
FORCE, NO TIRE SLIP ANGLE



- Lateral Force vs Slip Angle Maps:
- Aligning Torque vs. Slip Angle Maps:
- Camber Thrust Force vs Camber Angle Maps:
- Grip Value Maps:

ENHANCED TIRE MODEL:
- TIRE DATA LOOKUP TABLES
- TIRE DATA LOOKUP TABLES
- TIRE DATA TUNING PARAMETERS
- NON-LINEAR TIRE
LATERAL FORCE, NON-LINEAR TIRE
LATERAL FORCE, TOROUE, TIRE SUIP ANGLE
- Max. Grip µ = f (Fz, CS, Q, γ)





THE BASE TIRE MODEL IS PARAMETRIC AND BASED ON CORNERING STIFFNESS APPROACH (GRADIENTS). ALL TIRE DATA (CORNERING STIFFNESS, ALIGNING TORQUE STIFFNESS AND CAMBER THRUST) WILL BE SCALED FROM REFERENCE LOAD (STEPWISE) LINEAR TO IT'S VERTICAL LOAD @ OPERATING POINT.

THE COMBINED SLIP TIRE MODEL IS BASED ON ELEMENTARY FRICTION CIRCLE BEHAVIOUR, MEANING THAT AT ON LONGITUDINAL FORCE THE TIRE CORNERING STIFFNESS WILL BE MAXIMAL AND AT FULL LONGITUDINAL MUE SATURATION THE CORNERING STIFFNESS WILL BE MINIMAL.

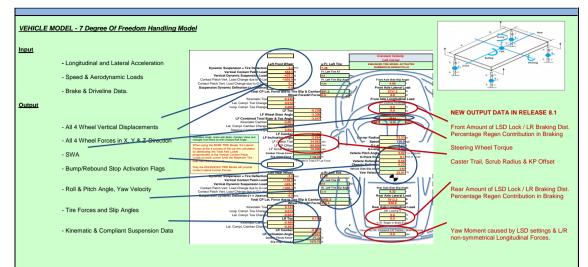
THE BASE TIRE MODEL DOES NOT PRODUCE ANY FORCES, TORQUES OR SLIP ANGLES. GRIP VALUE μ IS ALWAYS CONSTANT

THE ENHANCED TIRE MODEL DOES GENERATE OUT OF THE EQUATIONS FROM THE BASE TIRE MODEL NEW LOOK UP TABLES - AS A FUNTION OF TIRE SLIP ANGLE AND VERTICAL LOAD - FOR TIRE LATERAL FORCE RESP. TIRE ALIGINING TORQUE.

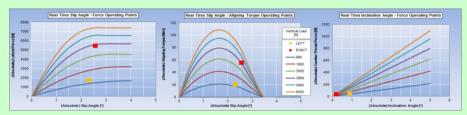
THE ENHANCED TIRE MODEL DOES ALLOW TO CALCULATE THE TIRE SLIP ANGLE AND DOES THEREFORE GIVE IN PARTICULAR MORE ACCURATE RESULTS AT THE NON-LINEAR HIGH-G OPERATING RANGE OF THE TIRE.

THE ENHANCED TIRE MODEL CAN ONLY BE USED IN CALCULATIONS. COMBINED WITH THE 7-DOF VEHICLE MODEL. STEP STEER AND FREQUENCY RESPONSE ARE UNAFFECTED AS THEY USE THE BASE TIRE MODEL ONLY.

Version 8.0 comes also with a specific knowledge/data base for Tire Data and a full plotting feature to visualize the Tire Characteristics in 2D & 3D Format.



- Tire Operating Points for the given Vehicle Condition:



The 7-DOF Vehicle Model does also create the Performance Envelope Graphs for G-Long & G-Lat as function of Velocity both for Traction as for Braking Conditions.

These Performance Envelopes are the fundamental enabler for the Laptime Simulation tool and describe the Combined G-G Performance Operating Range of the Vehicle.

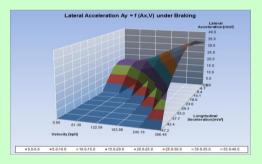
- One can choose to create the Velocity Data Points automatically of if desired enter Custom Points:

Automatically Calculated Data Points for Velocity [kph]	0.0	61.3	122.6	183.9	245.2	306.5	I Use Ouston Reference Velocity Points
Custom Data Points for Velocity - STAY WITHIN THE LIMITS!	0.0	120.0	160.0	180.0	220.0	306.5	Use custom Reference velocity Points

The Performance Envelopes can be created in 2 Different Modes:

CREATE LINEAR G-G-V MAP CREATE NON-LINEAR G-G-V MAP

- with the BASE Tire Model and a LINEAR Calculation (for a quick scan). This Simulation is less CPU-Time consuming, but more inaccurate.
- with the ENHANCE Tire Model and a FULL NON-LINEAR Calculation (this is the recommended, most accurate method).



DATA REFERENCE TABLE								
VELOCITY [kph]	Max. Ax TRACTION [g]	Max. Ax BRAKING [g]	Max. Ay LATERAL [g]					
61.3	1.053	1.599	1.650					
122.6	1.199	2.048	1.948					
183.9	1.184	2.759	2.377					
245.2	0.583	3.705	2.918					
306.5	0.065	4.807	3.229					

UNDERSTEER BEHAVIOUR - Bicycle Model for Linear Understeer Behaviour Speed, Aerodynamics Front and Rear Tire Data corresponding to the Vertical Load Condition at the Vehicle Operating Point INSTANTENEOUS Spring & Rollbar Settings (Roll Rates) Suspension Kinematics & Compliance Data. USER Defined Limits for Understeer & Vehicle Side Slip Angle Gradients (set 1000 to de-activate feature):

HINDEDSTEED BUINGET Maximum Understeer Gradient Limit during Cornering (US) 1000

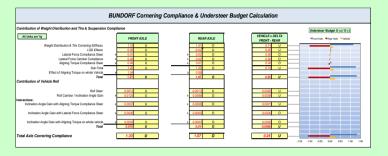
Maximum Fr. & Rr. Side Slip Angle Gradient Limit (SSA) 1000



⁻ Lateral Acceleration Sweep Setting (Constant Velocity vs. Constant Radius Procedure):
- Bundorf Compliance Setting (Will be automatically activated with BASE Tire Model & De-activated with ENHANCED Tire Model):



- Bundorf Comering Compliance & Understeer Budget Table: Linear Understeer Gradient considering Suspension Kinematics & Compliances AND IN RELEASE 8.1 LSD EFFECTS: Output

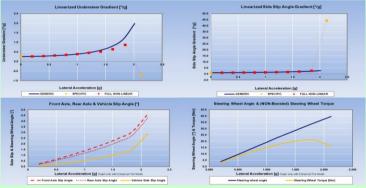


Input

Front & Rear Axle Cornering Stiffness:
 Linear Range Understeer Gradient (UG):
 Vehicle Slip Angle Gradient (SSAG):

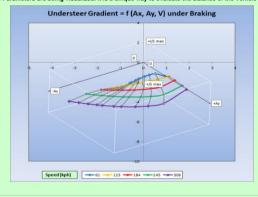


- Understeer Characteristics (UG,VG) for various lateral g-Levels based on Tire Load Characteristics & Roll Rates at those lateral g-Levels:



When using the Enhanced Tire Model, Axle Side Slip Angles and Steering Wheel Angle & Torque data from the 7-DOF Model can be plotted over the Lateral Acceleration Range.

The G-G-V-Map Procedure allows to create a 4 Dimensional "Understeer and Slip Angle Gradient" Performance Envelope where as a function of G-Long, G-Lat & Velocity, those Parameters are being visualized. It is a unique way to evaluate the Balance of the Vehicle in every possible operating condition.



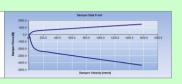
Gra	ph Refer	ence Dat	a Table
V [kph]	Ax [g]	Ay [g]	US Grad [°/g]
61	0.00	1.65	-0.7
61	-1.60	0.46	-16.9
123	0.00	1.93	1.7
123	-2.05	0.57	-11.0
184	0.00	2.38	1.7
184	-2.76	0.77	-6.3
245	0.00	2.94	0.8
245	-3.71	0.98	-3.1
306	0.00	3.29	-0.3
306	-4.81	1.24	-1.9

DAMPER TUNING - Percent Critical Damping & Ride Transfer Functions

Input

- Tire Vertical Stiffness & Suspension INSTANTANEOUS Wheel Rates (Straight Line Running vs. Cornering)
- Sprung & Unsprung Masses, Pitch Inertia
- Measured Damper Force/Velocity Data





- Damper Motion Ratio's & Scaling Factor:

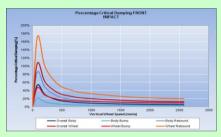
Fr. Damper to Wheel Motion Ratio	0.61	
Fr. Damping Scaling Factor	1.00 -	
(Permits Scaling of Fr. Linear Damping @ \	Wheel for Analysis)	

Output

- Damper Data @ Wheel:



- Curves for Percent Critical Damping for Body and Wheel in Compression and Rebound:

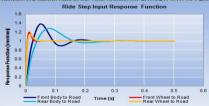


Activate / Re-Calculate Ride Step & Ride Frequency e-Activate Ride Step & Ride

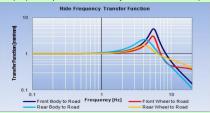
ONLY IN EXPERT VERSION:

- Ride Step Input Response with Damoed Oscillation Data in the Time Domain (DEACTIVATED BY DEFAULT IN ORDER TO SAVE CPU TIME). .

Ride Step Input Response Function



- Ride Frequency Transfer Function (FFT) with Amplification Factor and Dynamic Wheel Load Factor (DEACTIVATED BY DEFAULT IN ORDER TO SAVE CPU TIME).



SPRING TUNING - Natural Frequencies and Pitch & Bounce Center Calculation

Input - INSTANTANEOUS Wheel Rates for specified Load Condition

- Tire Vertical Rates for specified Load Condition

- Sprung & Unsprung Masses, Pitch Inertia

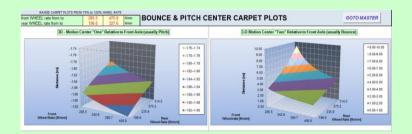
Output - Front & Rear Instantenous Ride Rates:

- Front and Rear Unsprung Mass Ride Frequencies:

- Bounce and Pitch Frequencies of the Sprung Mass:

- Bounce and Pitch Center Locations:

- Carpet Plots for Bounce & Pitch Center Locations



ROLLBAR TUNING - Mechanical Balance

Input - Front and Rear Suspension INSTANTANEOUS Roll Rates

- Front and Rear Instantenous Roll Center Heights

- Linear Roll Angle Gradient

Output

Output

- Roll couple Distribution:

- Suspension Load Transfer:
- Lateral Load Transfer Distribution:

- Bump & Rebound Stop Activation Info:

- Rollbar/Spring Rollrate Contribution:

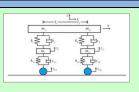
Heights	Output Parameter	RESULTS	
	Inst. Lat. Load Transfer Distribution	44.4	% front
	Inst. Roll Couple Distr. (Wheel Lift)	60.22	% front
	Instant. Roll Couple Distribution	60.22	% front
	Instant. L.L.T. Bias	2.04	% rel. to CoG
	Rollangle due to Spr. Mass Rollmoment	0.18	
	Rollangle @ Bump-Stop Activation	0.52]•
	Lateral G @ Bump-Stop	5.54	9
	Rollangle @ Rebound-Stop Activation	0.50	
	Lateral G @ Rebound-Stop		g
	(All in Pure Roll, no Lifting Effects of Roll Center Height)	
			AATET Ala

RESULTS - Sheet for Comparison of 2 or more Vehicles	2

<u>Input</u> All model data and results for the actual model and a reference data set.

Comparison of most important metrics and graphs. Sheet can be fully customized and used as a normal Excel Sheet.

Note: Data from a Reference Model can be exported or imported to/from an external EXCEL (*.xlsx) file.



<mark>╠┸┸┰┸╅╃╇┼┼┼┼┼┼┼</mark>

ONLY IN EXPERT VERSION: FREQUENCY STEER - Bicycle Model for Frequency Steer Response

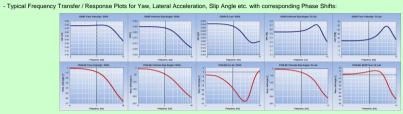
Input - Speed & Aerodynamics

Output

- Front and Rear Tire Data corresponding to the Vertical Load Condition at the Vehicle Operating Point

- Optionally Steering Wheel Angle, to be entered in the Master Control Sheet (which will acts as a TRIGGER for a Specific Calculation establishing the Vehicle Understeer Characteristics at the Lateral Acceleration corresponding to the given input SWA).





- W/O SWA = GENERIC Calculation: Metrics describing the most important Characteristics of Transfer Function Data:

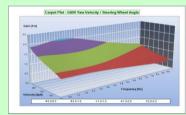
GENERIC FREQUENCY STEER RESPONSE DATA @ G-Long = 0g								
Frequency Steer Results Yaw Vel. / SWA Slip Angle / SWA G-Lat / SWA Slip Angle / G-Lat Yaw Vel. / G-Lat								
Frequency @ Peak	0.00 Hz	0.00 Hz	0.00 Hz	3.80 Hz	4.40 Hz			
Static Gain @ 0 Hz	0.969 1/a	0.030 -	0.057 g/*	0.519 %	16.863 */s/g			
Dyn. Overshoot @ Peak	0.00%	0.00% %	0.00% %	32.64% %	100.64% %			
Delay Time @ 1 Hz	27.6 ms	128.4 ms	53.5 ms	74.8 ms	-25.9 ms			

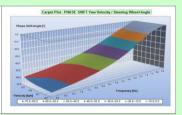
- W/SWA = SPECIFIC Calculation: Metrics for the Characteristics of the Transfer Function however now at the "Imposed" Lateral Acceleration corresponding to the given input SWA.

SPECIFIC FREQUENCY STEER RESPONSE DATA @ SWA = 15°, G-Lat = 0.7g, G-Long = 0g							
Frequency Steer Results		Slip Angle / SWA	G-Lat / SWA	Slip Angle / G-Lat	Yaw Vel. / G-Lat		
Frequency @ Peak	1.40 Hz	0.00 Hz	0.00 Hz	4.00 Hz	4.60 Hz		
Static Gain @ 0 Hz	0.798 1/s	0.022 -	0.047 g/°	0.472 °/g	16.863 °/s/g		
Dyn. Overshoot @ Peak	1.27% %	0.00% %	0.00% %	34.79% %	93.42% %		
Delay Time @ 1 Hz	22.4 ms	122.6 ms	46.0 ms	76.7 ms	-23.6 ms		

- Tables of all Key Metrics & Graphs for various Speeds presented in 2D and 3D Charts:





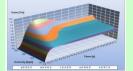


Ambridge)

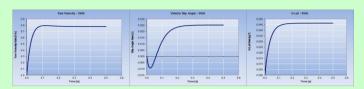
ONLY IN EXPERT VERSION: STEP STEER - Bicycle Model for Step Steer Response

Input - Speed & Aerodynamics

- Front and Rear Tire Data corresponding to the Vertical Load Condition at the Vehicle Operating Point
- Simulation Time for Step Response (0 2.5 sec)
- Optionally Steering Wheel Angle, to be entered in the Master Control Sheet (which will acts as a TRIGGER for a Specific Calculation establishing the Vehicle Understeer Characteristics at the Lateral Acceleration corresponding to the given input SWA).



Output - Typical Step Response Plots for Yaw, Lateral Acceleration, Slip Angle etc.:



- W/O SWA = GENERIC - Linear Step Steer Time Domain Data for Yaw Velocity, Vehicle Slip Angle and Lateral Acceleration & Corresponding Key Metrics

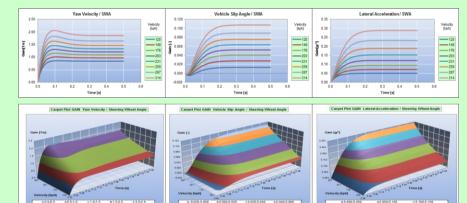
	GENERIC STEP STEER RESPONSE DATA @ G-Long = 0g							
- 0	Step Steer Response Data	Yaw Velocity Gain [1/s	Slip Angle Gain [-]	G-Lat Gain [g/°]	Simulation Time			
	90% Response Time	48.0 ms	180.0 ms	80.0 ms	0.50 s			
	Peak Value	0.796 1/s	0.025 -	0.046 g/°	Keep Simulation Time as short as possible			
	Time to reach Peak Value	118.0 ms	500.0 ms	454.0 ms	(Max 2.5s) ! If Results are incorrect/noisy			
	Dynamic Overshoot @ Peak	1.81% %	0.00% %	0.00% %	then reduce Maximum Simulation Time.			

- W/ SWA = SPECIFIC - Step Steer Time Domain Data, however now at the "Imposed" Lateral Acceleration corresponding to the given input SWA:

SPECIFIC STEP STEER RESPONSE DATA @SWA = 15°, G-Lat = 0.7g, G-Long = 0g								
Step Steer Response Data	Yaw [°/s]	Slip Angle [°]	G.Lat [g]	Simulation Time				
90% Response Time	54.0 ms	218.0 ms	70.0 ms	0.50 s				
Peak Value	12.099 1/s	0.335	0.700 g	Keep Simulation Time as short as possible				
Time to reach Peak Value	128.0 ms	500.0 ms	174.0 ms	(Max 2.5s) ! If Results are incorrect/noisy				
Dynamic Overshoot @ Peak	3.20% %	0.01% %	0.74% %	then reduce Maximum Simulation Time.				

- Tables of all Key Metrics & Graphs for various Speeds presented 2D and 3D Charts:

	YAW / SWA GAIN				SLIP ANGLE / SWA GAIN			G-LAT / SWA GAIN				
Speed [kph]	90% Response Time	Gain Peak Value	Time to reach Peak [ms]	Dynamic Overshoot @ Peak [%]	90% Response Time	Gain Peak Value	Time to reach Peak [ms]	Dynamic Overshoot @ Peak	90% Response Time	Gain Peak Value [9/*]	Time to reach Peak [ms]	Dynamic Overshoot @ Peak [%]
120	48.0	0.853	118.0	1.81%	180.0	0.013	500.0	0.00%	80.0	0.050	454.0	0.00%
148	46.0	1.006	110.0	3.85%	170.0	0.028	500.0	0.00%	102.0	0.071	438.0	0.00%
176	44.0	1.155	104.0	6.13%	164.0	0.040	478.0	0.00%	112.0	0.094	348.0	0.01%
203	42.0	1.305	98.0	8.28%	158.0	0.052	360.0	0.03%	116.0	0.121	304.0	0.05%
231	40.0	1.463	96.0	10.04%	154.0	0.063	336.0	0.08%	118.0	0.152	286.0	0.10%
259	38.0	1.634	94.0	11.22%	152.0	0.075	320.0	0.11%	120.0	0.188	284.0	0.13%
287	38.0	1.827	94.0	11.55%	152.0	0.089	330.0	0.09%	124.0	0.232	294.0	0.11%
314	40.0	2.052	96.0	10.80%	158.0	0.107	360.0	0.05%	134.0	0.288	332.0	0.05%

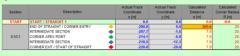


CIRCUIT LAYOUT - Create your own Test Track

2D Circuit Data. X & Y coordinates of "Driving Line".

5 Data Points per Corner.

2 Points for every Straight.





Circuit Graph, Distances and Cornering Radii Output



NOTE: Track data can be ex/-imported to/from and external EXCEL file in *,xlsx format.

LAPTIME CONTROL - CONTROL Sheet for Laptime Simulation

Input

- Laptime Simulation Control Data & Number of Iterations:
- Understeer Gradient & Vehicle Side Slip Angle Gradient Limits:
- Standing Start or Flying Lap Simulation:
- Simulation Control Panel:

Understeer Gradient Limit (US) Lim. Fr. & Rr. Side Slip Angle Gradient (SSA) Limit of Nr. of Iterations Laptime Module ON/OFF 1000.0 "/g 1000.0 "/g 250 [-] (default 250) 0 [-] switch (Y/N 1/0) ✓ Flying Lap



CREATE TIME HISTORY OF ALL VEHICLE CALCULATE / RE-RUNLAPTIME WITHOUT UPDATING G-G-V MAP CALCULATE NEW LAPTIME WITH UPDATED LINEAR G-G-V MAP CALCULATE NEW LAPTIME WITH UPDATED NON-LINEAR G-G-V MAP

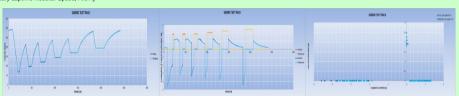
- Overal Laptime, Distance & Average Speed: Output



- Sector Times & Sector Data,



- Elementary Laptime Results: Speed, Ax, Ay



- A full Time History Data Set of all Dynatune Metrics can be created for a Laptime Simulation

In Version 8.0 a Laptime Sensitivity Study can be executed with up to 20 Pre-Defined - typically "Track-Use" - Setup Parameters:



LAP RESULTS - Sheet for Comparison of Laptime results of 2 vehicles

Input Time History Data Set of a Laptime Simulation for the actual model and a reference data set .

Output Comparison/Time History of all Dynatune R&H metrics and selected graphs of 2 Setups for Lap Simulation. Sheet can be fully customized.

Note: Data from a Reference Lap can be exported to an external EXCEL(*.xlsx) file.

10 EASY STEPS TO HAPPY SIMULATIONS IN DYNATUNE

1) REMEMBER THAT THE WORKBOOK IS COPY PROTECTED. ONLY THE USER SHEET AND RESULT SHEETS ARE UNPROTECTED AND ALLOWED TO BE CUSTOMIZED BY THE USER. EACH VERSION OF DYNATUNE HAS ITS OWN FEATURES ENABLED/DISABLED. THE PROTECTION SOFTWARE WILL ALLOW TO SAVE A CUSTOM VERSION OF THE WORKBOOK ON EXIT.

2) THE WORKBOOK IS BASED ON ANALYTICAL EQUATIONS. THIS IS IT'S STRENGTH FOR VELOCITY - HOWEVER. IF YOU ENTER NUMBERS THAT FOR SOME PHYSICAL REASON DO NOT MAKE SENSE OR CREATE SINGULARITIES THE WORKBOOK CAN SHOW "#NUMBER" - SOMETIMES NOT RECOVERABLE. WHEN THIS HAPPENS FIRST RUN THE START/INITIALISE PROCEDURE WHICH SHOULD RESOLVE THE PROBLEM.

3) ALL RELEVANT INPUT FIELDS HAVE BEEN PROVIDED WITH SENSIBLE PHYSICAL LIMITS IN ORDER TO AVOID SINGULARITIES IN THE CALCULATION. SINCE A NOVICE COULD PRODUCE CASE 2) IT IS HOWEVER STRONGLY RECOMMENDED TO MAKE A COPY OF THE ORIGINAL SHEET IN WINDOWS EXPLORER FOR REFERENCE. SEE 1)

4) DO READ THE "README PAGE" AND MAKE SURE THAT YOU HAVE FOLLOWED ALL MENTIONED RECOMMENDATIONS. MOST OF ALL MAKE SURE THAT YOUR TIRE DATA ARE CORRECT FOR THE OPERATING POINT VERTICAL LOAD CONDITION THAT YOU DO WANT TO INVESTIGATE

5) THE TIRE MODEL IS BASED ON ALGORITHMS OF CORNERING STIFFNESS IN FUNCTION OF VERTICAL, LATERAL & LONGITUDINAL LOAD AND HAS BEEN KEPT AS LEAN AS NECESSARY IN ORDER TO AVOID TO GO TO COMPLEX PACELKA INTERPOLATIONS OR OTHER TIRE-MODELS. VERIFY WHETHER YOUR TIRES ARE OPERATING IN THE CORRECT LOAD RANGE.

6) DYNATUNE HAS BEEN SPECIFICALLY DEVELOPED AND ADAPTED TO MS EXCEL, ESPECIALLY FOR USING THE STANDARD ITERATION PROCEDURE OF EXCEL, BEAR IN MIND, THAT THE EXCEL ITERATION ALGORITHM IS NOT AS PERFECT AS SOME SOPHISTICATED COMMERCIALLY AVAILABLE SOLVERS, SO PAY IN PARTICULAR ATTENTION WHEN EXECUTING CALCULATIONS WHILST USING BUMP STOPS. MAKE SURE THAT ALL RATE CHANGES ARE SMOOTH. ALL CALCULATIONS ARE PROGRAMMED IN SUCH A WAY THAT THE CALCULATIONS WILL ALWAYS FINISH. SEE ALSO 7)

7) AS LONG AS YOU DO NOT USE BUMP-STOPS OR RIDEHEIGHT DEPENDENT AERODYNAMICS, YOUR CALCULATIONS WILL BE STRAIGHT FORWARD. ONCE ENTERING INTO NON-LINEARITY OF THOSE FEATURES AND THUS BY PHYSICS ENFORCED NECESSARY "CIRCULAR" ITERATIONS YOUR SOLVER TIME WILL INCREASE S. DO USE THESE ONLY IF YOU WANT OR NEED TO DO SO.

8) IF ACTIVATED, THE RIDE FREQUENCY TRANSFER FUNCTION WILL SLOW ALL CALCULATIONS DOWN, SINCE IN THE BACKGROUND VERY COMPLEX (I) FFT CALCULATIONS HAVE TO BE EXECUTED AT EACH ITERATION. DO ONLY USE THIS SWITCH IF YOU WANT TO INVESTIGATE THIS PARTICULAR MATTER AND TURN IT OFF AGAIN WHEN NOT NEEDED

9) UNDERSTANDING THE WORD "LINEAR" & "GENERIC" IN CHASSIS DYNAMICS

A) LINEAR BEHAVIOR OF A SYSTEM: THIS SIGNIFIES THAT THE RESPONSE OF THE SYSTEM IS ALWAYS DIRECTLY PROPORTIONAL TO THE INPUT (EITHER "1" OR "10") WITHOUT ANY CHANGE OF STATE OF YOUR SYSTEM (ALL PARAMETERS REMAIN LINEAR & UNCHANGED). DUE TO THE LINEARITY THESE SYSTEMS CAN BE ANALYZED "GENERICALLY" AND PERMIT

LINEAR EXTRAPOLATION TOWARDS A PARTICULAR CONDITION (PREDICTION).

NON-LINEAR BEHAVIOR OF A SYSTEM: THIS SIGNIFIES THAT THERE IS NO DIRECT PROPORTIONAL RESPONSE CAUSING USUALLY A CHANGE OF STATE WHICH MAKES A"SPECIFIC'
INVESTIGATION AROUND THIS POINT NECESSARY. A NUMERICAL ITERATION IS NECESSARY TO APPROACH THIS POINT OF NON-LINEARITY, IT CANNOT BE PREDICTED BY LINEAR
EXTRAPOLATION.

B) LINEAR TIRE BEHAVIOUR: MEANS THAT THE TIRE CHANGES LINEARLY ITS MAJOR CHARACTERISTICS LIKE F.I. CORNERING STIFFNESS WITH LOAD & SLIP ANGLE NON-LINEAR TIRE BEHAVIOUR: STARTS BECOMING NOTICEABLE USUALLY ABOVE 0,5 - 0,7 G LATERAL ACCELERATION CAUSING A NON-LINEAR CHANGE OF TIRE CORNERING STIFFNESS. THIS BEHAVIOUR CAN BE SIMULATED BY CHANGING LINEAR CHARACTERISTICS STEPWISE OVER OPERATING RANGE (=PARTIALLY LINEARIZED).

C) <u>LINEAR SUSPENSION CHARACTERISTICS</u>: BOTH (ELASTO-)KINEMATICS & VERTICAL WHEEL RATE ARE LINEAR.

NON-LINEAR WHEEL RATES (=BUMP-STOPS) PROVOKE NON-LINEAR VERTICAL FORCE REACTIONS WHICH WILL RESULT IN A DIFFERENT TIRE BEHAVIOR, EFFECTIVELY CAUSING A CHANGE OF STATE WHICH REQUIRES ITERATIONS. NOT USING BUMP-STOPS WHILST CORNERING WILL KEEP YOUR SUSPENSION LINEAR & THEREFORE THE TIRE MORE LINEAR.

D) LINEAR RANGE UNDERSTEER: UNDERSTEER IN THE LINEAR RANGE OF VEHICLE DYNAMICS - THIS RANGE IS PRIMARILY DEFINED BY THE LINEAR RANGE OF THE TIRE AND CAN D) LINEAR RANGE UNDERSTEER; UNDERSTEER IN THE LINEAR RANGE OF VEHICLE DYNAMICS- THIS RANGE IS PRIMARILY DEFINED BY THE LINEAR RANGE OF THE TIRE AND CAN
GO - DEPENDING ON THE TIRE - UP TO 0, 76, THE LINEAR RANGE DEFINES ALL ON-CENTER HANDLING CHARACTERISTICS & BASIC TRANSIENT STABILITY OF A VEHICLE.
IMPORTANT NOTE 1): LINEAR RANGE UNDERSTEER CANNOT BE SENSED BY DRIVERS. THE TYPICAL DRIVER SENSED UNDERSTEER IS THE NON-LINEAR RANGE UNDERSTEER.
IMPORTANT NOTE 2): A VEHICLE WITHOUT LINEAR RANGE UNDERSTEER IS PHYSICALLY NOT STABLE AND CANNOT BE ANALYZED I

NON-LINEAR RANGE UNDERSTEER; UNDERSTEER IN THE RANGE WHERE ETHER TIRE OR SUSPENSION OR ROTHED RECOME SIGNIFICANTLY NON-LINEAR (HIGH G-LOADS). THE NONLINEAR UNDERSTEER BEHAVIOR AT HIGH G CAN BE SIGNIFICANTLY DIFFERENT FROM THE LINEAR RANGE AND CAN BE "UNDERSTEERING", "OVERSTEERING" OR "NEUTRAL".

10) USE THE SIMULATION BUTTONS ON THE MASTER SHEET CORRECTLY

A) AFTER ENTERING DATA DO ALWAYS. RUN THE "START/INITIALISE" PROCEDURE. THIS WILL CALCULATE ALL INITIAL SETTINGS AND VERIFY WHAT PHYSICAL LIMITS ARE APPLICABLE TO THE VEHICLE. YOU WILL SEE THESE LIMITS AS LIMITS FOR THE SIMULATION. THE PROCEDURE WILL SET G-LAT, G-LONG, SWA TO ZERO & SET THE VELOCITY TO 120KPH. ALSO DEFAULT DYNATUNE ITERATION VALUES WILL BE (RE-)SET

B) THE "GO GENERIC" PROCEDURE WILL CREATE GENERIC RESULTS (G-LAT=0/SWA=0) FOR LINEAR RANGE UNDERSTEER BEHAVIOR, FREQUENCY STEER RESPONSE AND STEP STEER TEST. ONE CAN MODIFY ONLY "SPEED" AND "G-LONG" (IN ORDER TO SIMULATE THE EFFECTS OF AERO & LONGITUDINAL WEIGHT TRANSFER ON VERTICAL AXLE LOAD CHANGES AND THUS ON THE LINEAR LATERAL DYNAMIC BEHAVIOR OF THE TIRE). ONE CANNOT MODIFY THE STEERING WHEEL ANGLE. THE GENERIC CALCULATION DOES NOT PERMIT A CHANGE OF STATE OF THE MODEL MEANING THAT IN PARTICULAR WHEEL RATES REMAIN CONSTANT AS BEING CALCULATED AT THE START OF THE LATERAL PORTION OF THE CALCULATION.

THE LINEARIZED UNDERSTEER BUDGET CALCULATION FROM 0 TO G-LAT-MAX IS BASED ENTIRELY ON THIS PRINCIPLE AND MERELY CONSIDERS THE EFFECT OF LINEAR LATERAL LOAD TRANSFER ON TIRE CHARACTERISTICS (=CORNERING STIFFNESS) AND THE CONSEQUENT EFFECT ON UNDERSTEER.

C) THE "GO SPECIFIC" PROCEDURE WILL ALLOW TO ENTER "G-LAT", "G-LONG", "SPEED" & "SWA" IN ORDER TO INVESTIGATE ONE SINGLE SPECIFIC CONDITION ALLOWING ANALYSIS OF THE RESULTS FOR ALL 4 CORNERS OF THE VEHICLE IN THAT CONDITION. IN THE "SPECIFIC" CALCULATION A CHANGE OF STATE OF THE MODEL - REFLECTING FOR INSTANCE WHERE RATE CHANGES DUE TO A BUMPSTOP : BY OSSIBLE. SINCE A CHANGE OF STATE IS PERMITTED THE RESULTS FORM C) CAN DEFER SIGNIFICANTLY FROM B). THE GO SPECIFIC PROCEDURE TRIES IN "ONE" SINGLE STEP TO ACHIEVE THE TARGETED VALUES FOR G-LAT & G-LONG AND BUT IF NOT SUCCESFULL - DUE TO ANY EXCEEDING OF LIMITS (I.E. FOR UNDERSTEER / OVERSTEER) - IT WILL TRY TO APPROACH THAT LIMIT. IF YOUR MODEL CONTAINS SEVERE NON-LINEARITIES IT IS ALWAYS RECOMMENDED TO RUN THE "FULL NON-LINEAR" SWEEP WHICH WILL CONSIDER ALL POSSIBLE BOUNDARIES AND MORE IMPORTANTLY WILL DOCUMENT THEM IN MORE SIMULATION STEPS.

THE RESULTS OF ALL 4 CORNERS WILL BE USED FOR CALCULATING THE EFFECTIVE AXLE CORNERING STIFFNESS'S WHICH WILL BE USED BY THE BICYCLE MODEL. IF HOWEVER NO CHANGE OF STATE OCCURS (I.E NO BUMPSTOP ACTIVATION) THE RESULTS OF THE SPECIFIC CALCULATION WILL BE EQUAL TO THE GENERIC ONE.

DO NOTE THAT A SPECIFIC STEERING WHEEL ANGLE (SWA) INPUT WILL ONLY AFFECT THE "STEP STEER" & "FREQUENCY STEER" PROCEDURE CHANGING THEM FROM "GENERIC" RESULTS TO "SPECIFIC" RESULTS <u>FOR ONE PARTICULAR LATERAL ACCELERATION</u> WHICH IS CORRELATED TO THE IMPOSED STEERING WHEEL ANGLE.
ALSO DO NOTE THAT DIFFERENT FROM ALL ABOVE A CHANGE OF STATE OF THE MODEL IS FOR THESE TYPE OF CALCULATIONS <u>NOT</u> POSSIBLE (LINEAR BICYCLE MODEL).
ENTERING A SPECIFIC SWA WILL ALLOW A FAST COMPARISON WITH MEASURED TEST DATA—WHICH ARE USUALLY RECORDED FOR A DEFINED SWA OR A DEFINED LATERAL ACCELERATION. SPEED AND G-LONG ARE AGAIN FREE TO BE CHANGED IN ORDER TO SIMULATE THEIR EFFECT ON VERTICAL AXLE LOAD & CORNERING STIFFNESS

D) THE "GO FULL NON-LINEAR" PROCEDURE REPEATS BASICALLY THE "GO-SPECIFIC" PROCEDURE FROM "0" TO "G-LAT-MAX" IN 10 STEPS. THIS G-LAT-MAX WILL BE ALWAYS APPROACHED BY THE PROGRAM <u>AUTOMATICALLY</u> BASED ON EITHER PHYSICAL LIMIT'S OR BY EXCEEDING THE IMPOSED LIMITS FOR MAXIMUM UNDERSTEER/OVERSTEER. ALL RESULTS WILL BE SAVED FOR EACH INTERMEDIATE STEP IN THE "RESULTS" SHEET. THE "GO FULL NON-LINEAR" PROCEDURE WILL PERMIT DETAILED ANALYSIS OF THE WHOLE RANGE OF LATERAL ACCELERATION

E) THE "CLEAR FULL NON-LINEAR" PROCEDURE WILL ERASE ALL THE RESULTS FROM THE "GO FULL NON-LINEAR" PROCEDURE

F) THE "SET DATA REFERENCE" PROCEDURE WILL COPY ALL OF YOUR EXISTING "ACTUAL" MODEL DATA IN THE "RESULTS" SHEETS TO THE "REFERENCE" COLUMN AS VALUES THIS PERMITS AN EASY COMPARISON BETWEEN TWO VEHICLES. REVERTING THE PROCEDURE CAN BE DONE WITH THE "LOAD DATA REFERENCE" PROCEDURE WHICH WILL COPY ALL INPUT DATA FROM THE REFERENCE DATA SET TO THE ACTUAL DATA BEING USED.

G) THE "EXPORT REFERENCE DATA" PROCEDURE WILL EXPORT ALL OF YOUR "REFERENCE" MODEL DATA IN THE "RESULTS" SHEETS TO AN EXTERNAL EXCEL SHEET IN .XLSX FORMAT. VICE VERSA THE "IMPORT REFERENCE DATA" PROCEDURE WILL IMPORT A PREVIOUSLY CREATED "EXPORT" DATASET ON TO THE REFERENCE DATA.

F9 however still works and can be used when working in detailed tuning sheets

AND ANOTHER 10 STEPS FOR HAPPY LAPTIME SIMULATION

1) APPLY ALL 10 PREVIOUS STEPS FROM HAPPY SIMULATIONS. STRICTLY

2) THE EASIEST TRACKS ARE LIKE THE INCLUDED "GENERIC" TRACK - BRAKE ON THE STRAIGHT AND THEN CORNER TO THE MAX. ALL OTHER COMBINATIONS ARE MORE DEMANDING BOTH FOR THE DRIVER AS FOR THE CALCULATION. REMEMBER THAT.

3) KEEP TRACKS AS SHORT AS POSSIBLE. DO NOT USE 20 CORNERS JUST BECAUSE YOU CAN. A QUICK SCAN ON 4 REFERENCE CORNERS WILL OFTEN GIVE ALSO GOOD INDICATIONS.

4) WHEN RUNNING A NEW TRACK FOR THE FIRST TIME, THE STANDARD 250 ITERATIONS WILL NOT BE SUFFICIENT TO CONVERGE TO A ROBUST SO LUTION. THE MORE COMPLEX THE TRACK, THE MORE NON-LINEAR THE CAR, THE MORE TIME IS NEEDED. DEPENDING ON YOUR HARDWARE INCREASE ITERATIONS TO 10.000 AND LET IT RUN FOR AWHILE. REPEAT IF NECESSARY.

5) ALWAYS VERIFY THE LAPTIME RESULT BY RUNNING AN ADDITIONAL STANDARD RUN (250 ITERATIONS) IN ORDER TO VERIFY THAT THE LAPTIME DOES NOT CHANGE ANYMORE INDICATING THAT THE OPTIMIZATION PROCEDURE HAS FINISHED CORRECTLY.

6) TRY TO AVOID A "NON-LINEAR" CAR WITH BUMPSTOPS ACTING IN CORNERING. A LINEAR CALCULATION IS A LOT FASTER THAN A NON-LINEAR.

7) THE BASE TIRE MODEL IS A LOT FASTER THAN THE ENHANCED TIRE MODEL. WITH RESPECT TO LAPTIMES THE DIFFERENCES BETWEEN THE TWO TIRE MODELS ARE MARGINAL AND DIFFERENCES ARE SOLELY DUE TO LIMIT UNDERSTEER GRADIENT BEHAVIOUR. IF YOU ARE NOT INTERESTED IN DETAILED UNDERSTEER ANALYSIS. USE BASE TIRE MODEL.

8) UNLESS YOU ARE INTERESTED IN CORRELATING THE UNDERSTEER LIMITS OF THE MODEL TO DRIVER PERCEPTION LET THE LIMITS FOR UNDERSTEER GRADIENT AND VEHICLE SIDE SLIP ANGLE GRADIENT AS HIGH AS POSSIBLE. THIS WILL AVOID MANY ITERATIVE CALCULATIONS TOWARDS THE IMPOSED LIMITS FOR THEM.

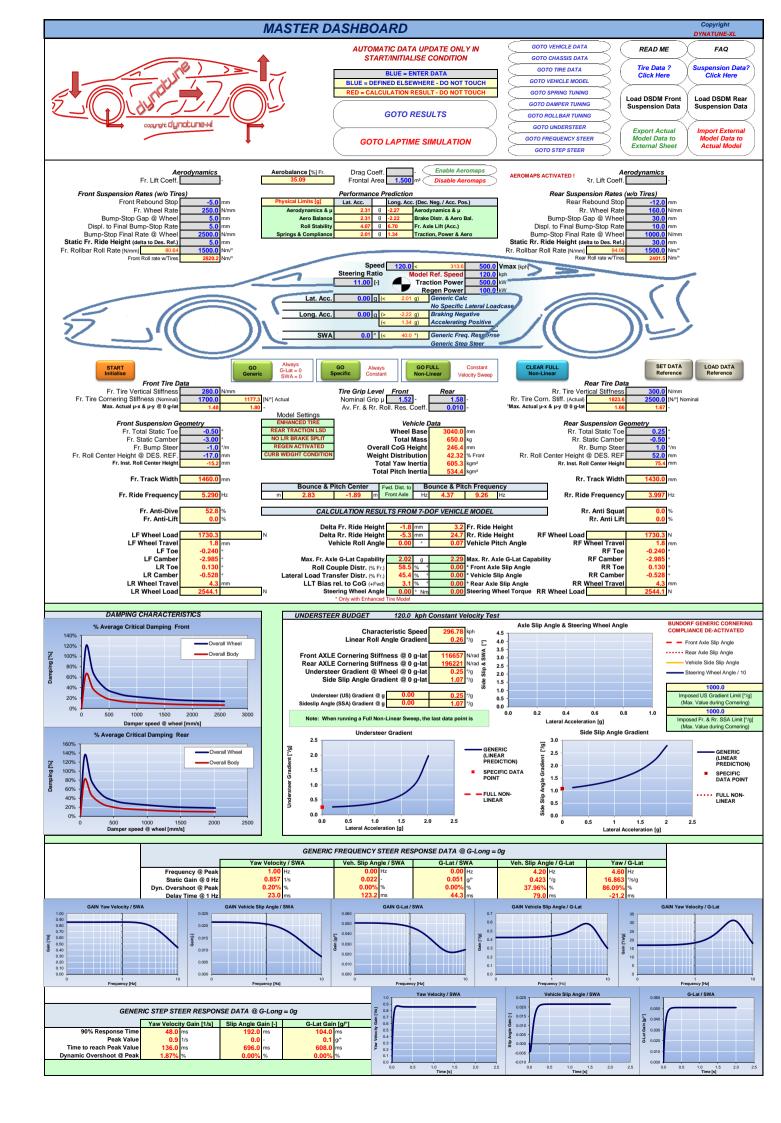
9) DO NOT RUN TIME HISTORY CALCULATIONS UNLESS YOU ARE SURE YOU WANT TO. THE TIME HISTORY CALCULATION WILL TAKE EVERY DATAPOINT OF THE LAPTIME SIMULATION AND RUN IT AS A "SPECIFIC" CALCULATION CREATING ALL DATA FOR THAT SPECIFIC POINT. DO ONLY DO THIS IF YOU ARE SURE THAT YOU NEED THIS INFORMATION.

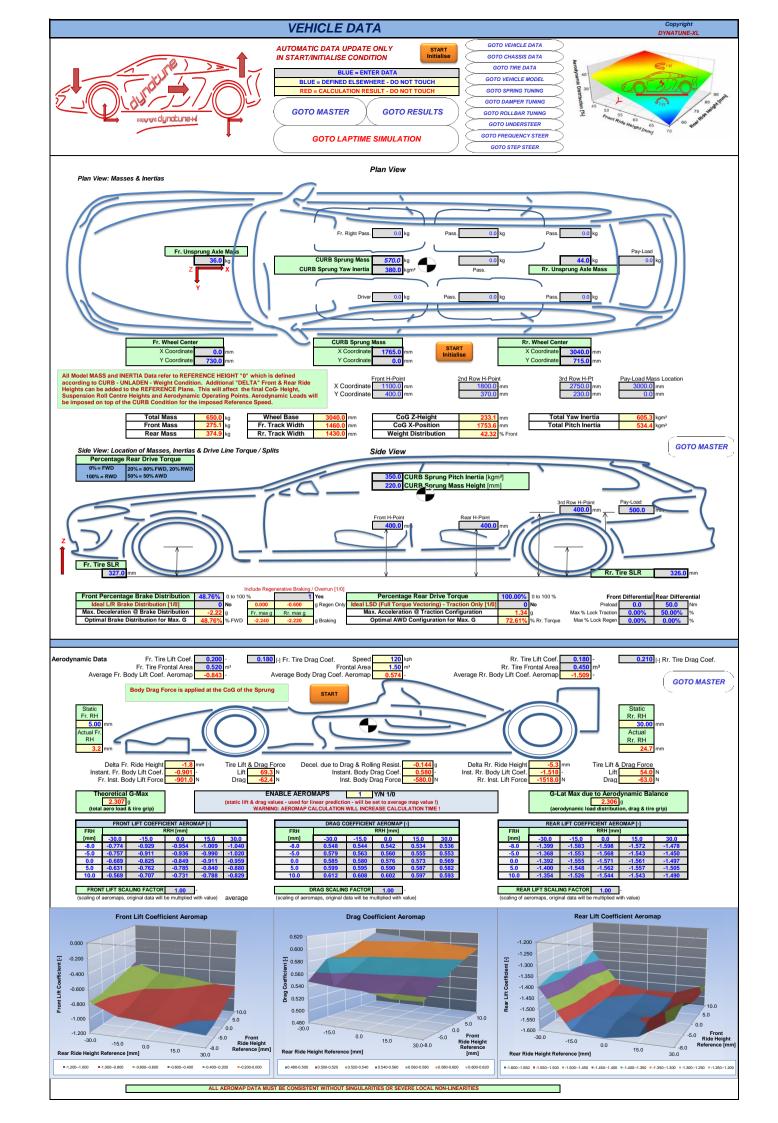
10) REMEMBER THAT THE MORE COMPLEX YOUR MODEL IS (BUMP-STOPS), THE MORE COMPLEX YOUR TIRE MODEL IS (ENHANCED vs. BASE), THE MORE COMPLEX YOUR TRACK IS AND THE TIGHTER YOUR UNDERSTEER GRADIENT / SIDE SLIP ANGLE GRADIENT LIMITS ARE THE MORE TIME YOUR SIMULATION WILL TAKE. CREATING A NON-LINEAR PERFORMANCE ENVELOPE WILL TAKE BY ITSELF APPROXIMATELY 2.5 TIMES MORE CPU TIME THAN THE BASE TIRE MODEL. TISHTHING UP THE LIMITS FOR UNDERSTEER GRADIENT / SIDE SLIP ANGLE GRADIENTS WILL INCREASE SIGNIFICANTLY THE NUMBER OF ITERATIONS IN ORDER TO FIND THE ACCORDING AX, AY POINTS ON THE PERFORMANCE ENVELOPE.

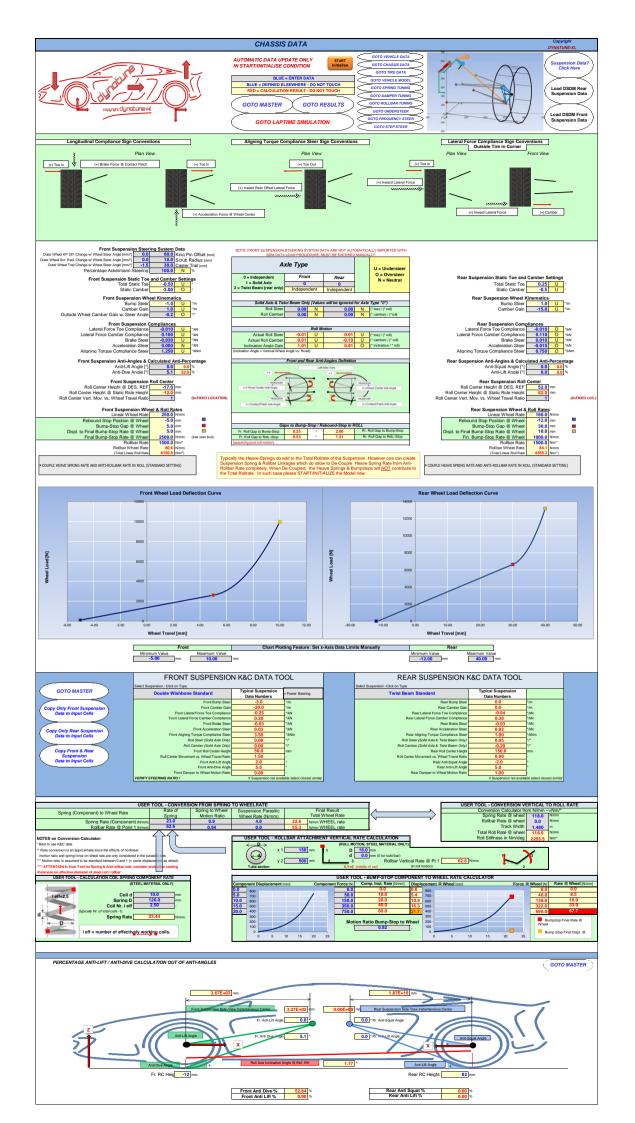
UNPROTECTED SHEET FREE FOR USAGE - CANNOT BE RENAMED
Can be used as normal Excel Sheet.
DO NOT DELETE "EXPORT" BUTTON

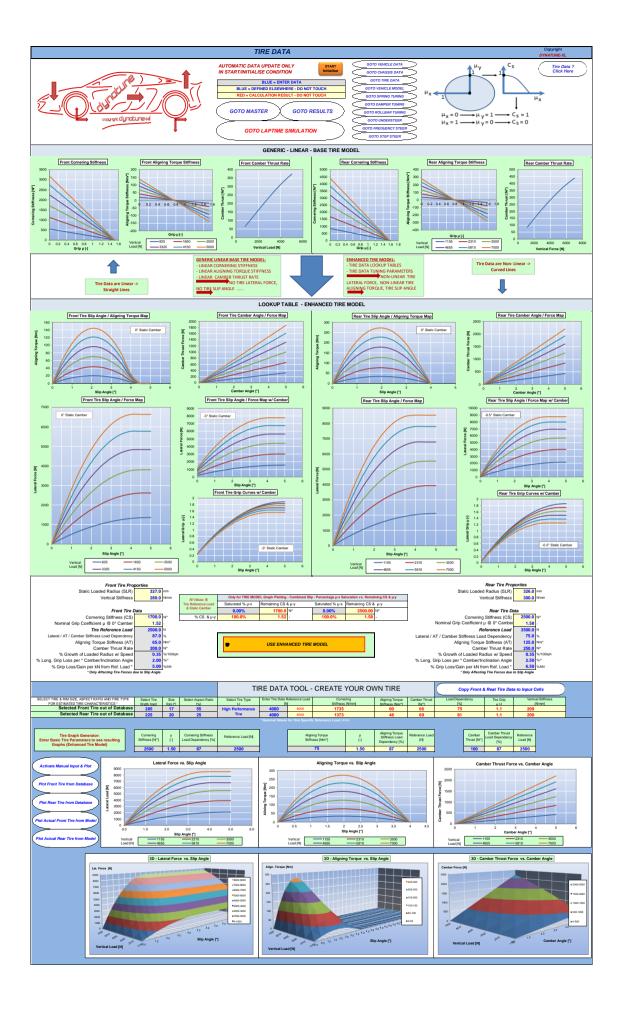
EXPORT COMPLETE USER SHEET

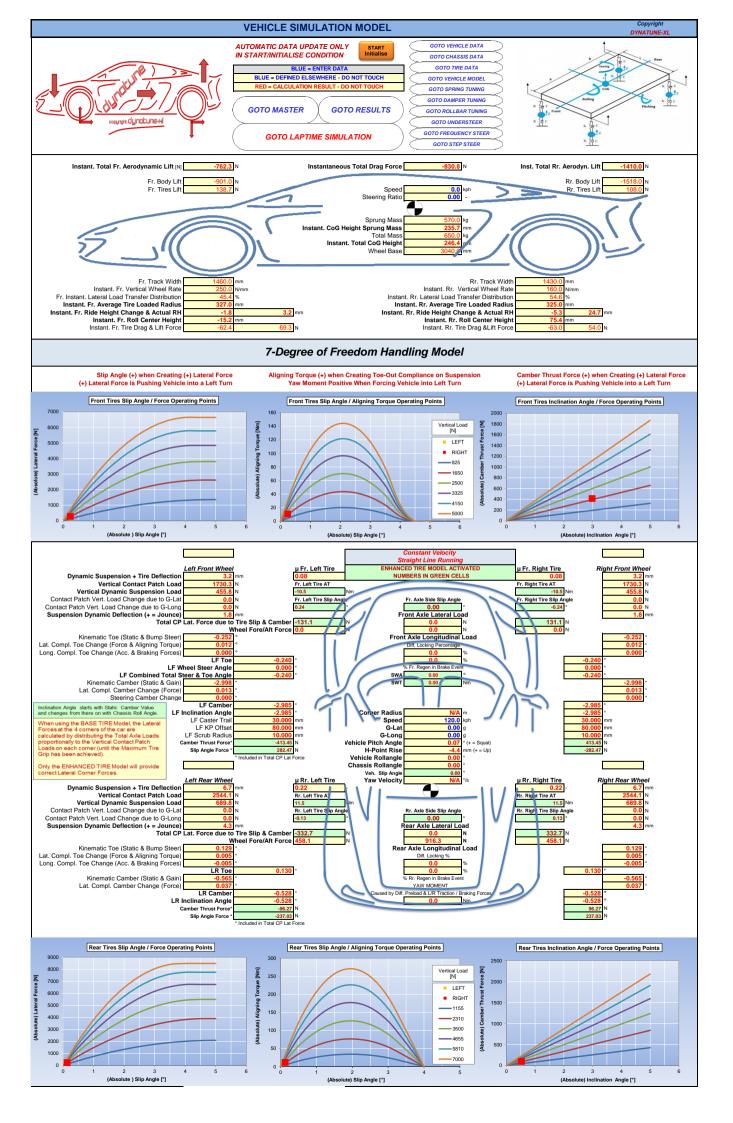
E	cample of Cu	stom USER F	ost-Process	ing for Steer	ing Wheel To	orque as Fun	ction of Later	ral Acceleration
IPUT DAT	A FROM SDN	1						
			Nominal Trail	35	mm		0.035	m
(Caster Trail Char	nge with Steer (d	direction toe-in)	-1.5	mm/deg		-0.0015	m/deg
	Caste	r Trail Change i	n Jounce travel	0	mm/mm		0	m/mm
		_			_			<i>!</i>
l	Data from RE	SULTS Shee	et from Later	al Accelerati	on Sweep Ca	alculation - O	nly Fy, No F	Contribution
G-Lat*	(Abso	lute) Steering	Aligning Torq	ue Data Front	Axle - LEFT 1	TURN CORNER	? [Nm]	Steering Wheel Torq
[g]	Left Fy AT	Left Tire AT	Left Total AT	Right Fy AT	Right Tire AT	Right Total AT	Total Axle AT	[Nm]
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.20	4.79	9.41	14.20	14.80	10.75	25.56	39.75	3.61
0.40	12.57	17.16	29.73	25.90	22.30	48.20	77.93	7.08
0.60	19.60	22.40	42.00	37.86	33.10	70.96	112.96	10.27
0.80	25.82	26.26	52.08	50.63	44.25	94.87	146.95	13.36
1.00	30.95	27.94	58.89	63.87	53.91	117.78	176.66	16.06
1.20	35.04	27.70	62.74	77.82	61.72	139.54	202.29	18.39
1.41	38.03	25.84	63.88	92.52	67.18	159.70	223.57	20.32
1.62	39.95	21.91	61.87	108.18	67.60	175.78	237.65	21.60
1.85	40.46	15.25	55.71	124.35	57.10	181.45	237.17	21.56
2.12	39.62	0.00	39.62	142.85	0.00	142.85	182.47	16.59
t G-Lat = 0 a	Il calculated value	s are set to 0. Or	-Centre Data ava	ailable in Vehicle	Model Sheet			
	Steering Alig	ning Torque Dat	a @ Front Axle		Steering Wheel Torque LEFT TURN CORNER			
250.0		I I TORRECOR	*LIX		25.0		22.7.70.0.70	OHILEK
250.0					20.0			
200.0					<u> </u> 15.0 -			
150.0					ž			
100.0			\leq		o 10.0			
100.0					5.0			
0.0	0.3 0.5	0.8 1.0 1.3	1.5 1.8	2.0 2.3	0.0			
		eral Acceleration			0.0	0.3 0.5	0.8 1.0 1.3	3 1.5 1.8 2.0 2.3
	ft Fy AT •	Left Tire AT		ht Fy AT	0.0		ateral Accelerat	
	tht Tire AT	Total Axle A						



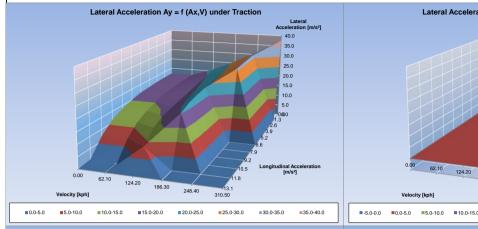


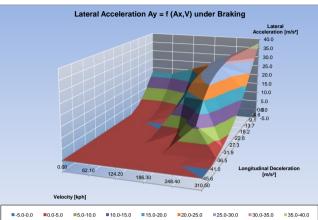


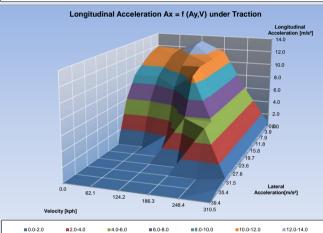


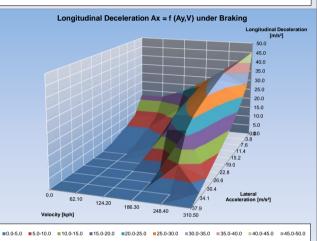










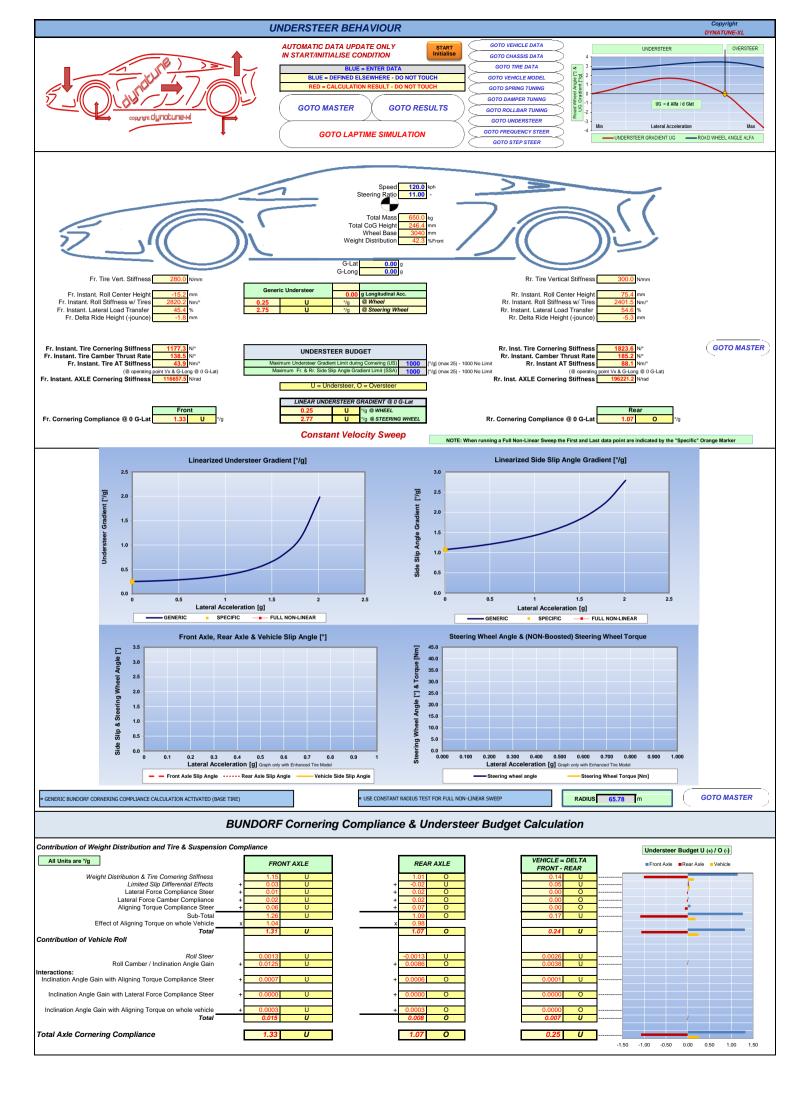


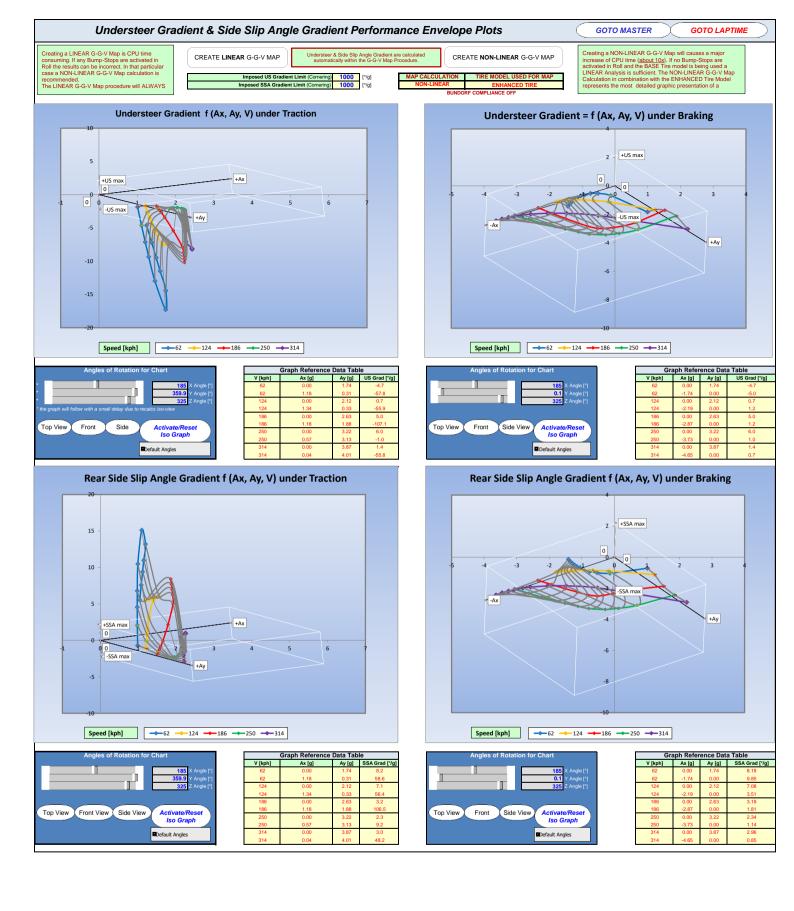
DATA REFERENCE TABLE						
VELOCITY [kph]	Max. Ax TRACTION [g]	Max. Ax BRAKING [g]	Max. Ay LATERAL [g]			
62.1	1.179	1.743	1.743			
124.0	1.337	2.189	2.123			
186.3	1.177	2.873	2.629			
249.5	0.566	3.735	3.224			
313.5	0.036	4.646	3.868			

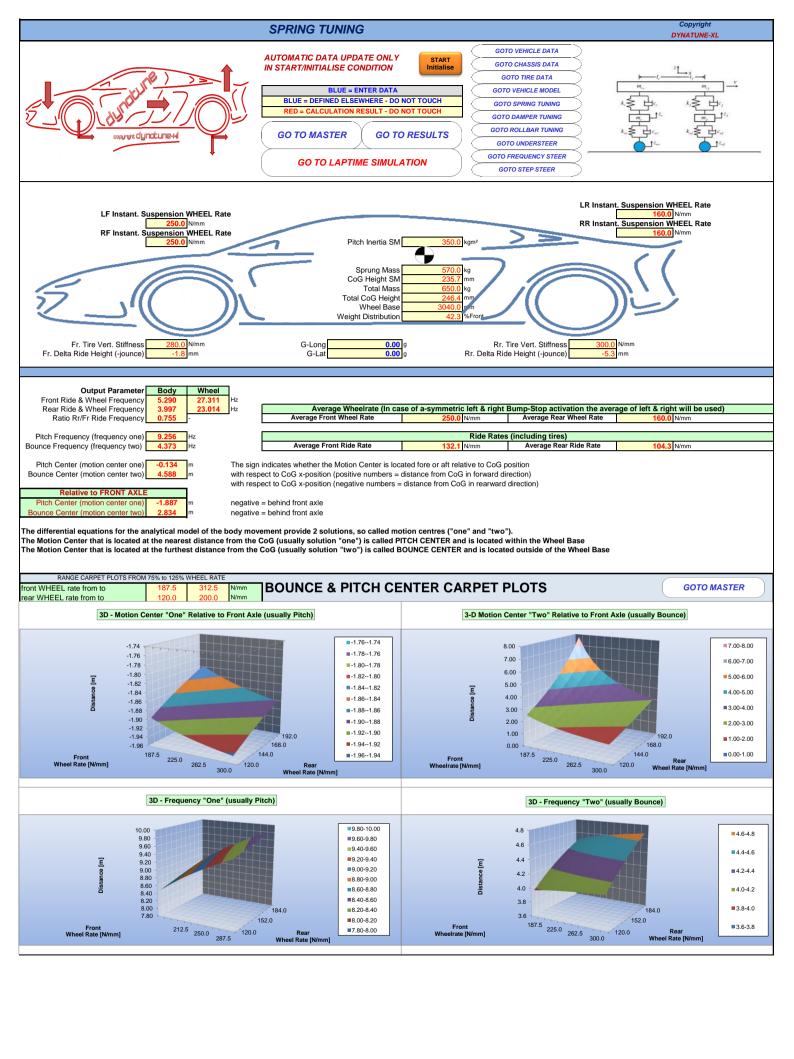
GOTO MASTER

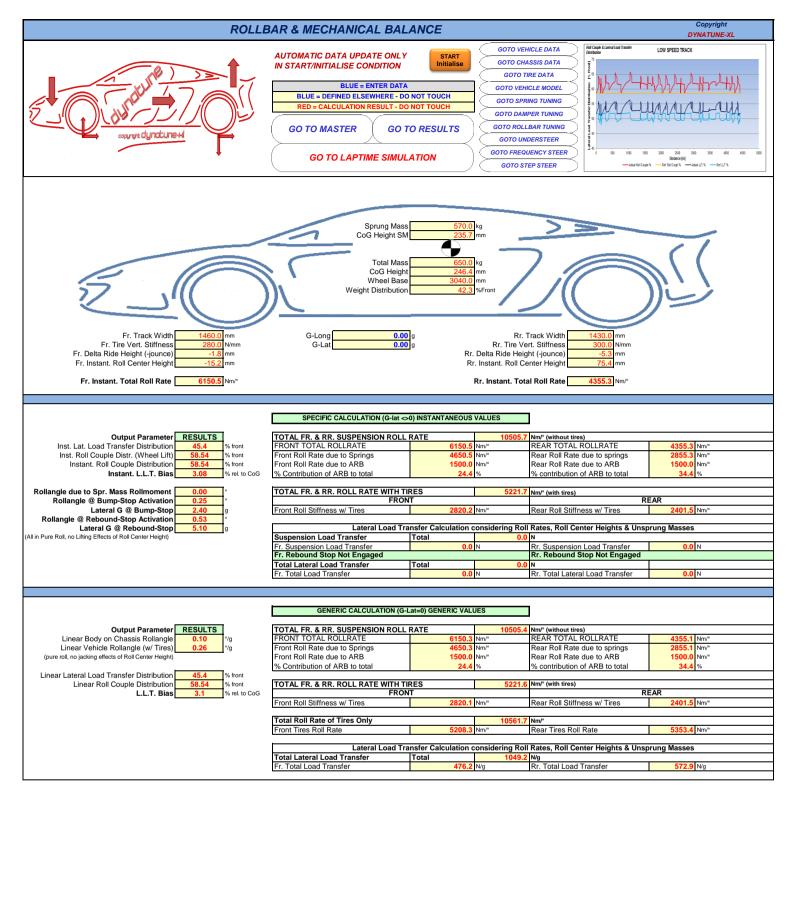
GOTO LAPTIME

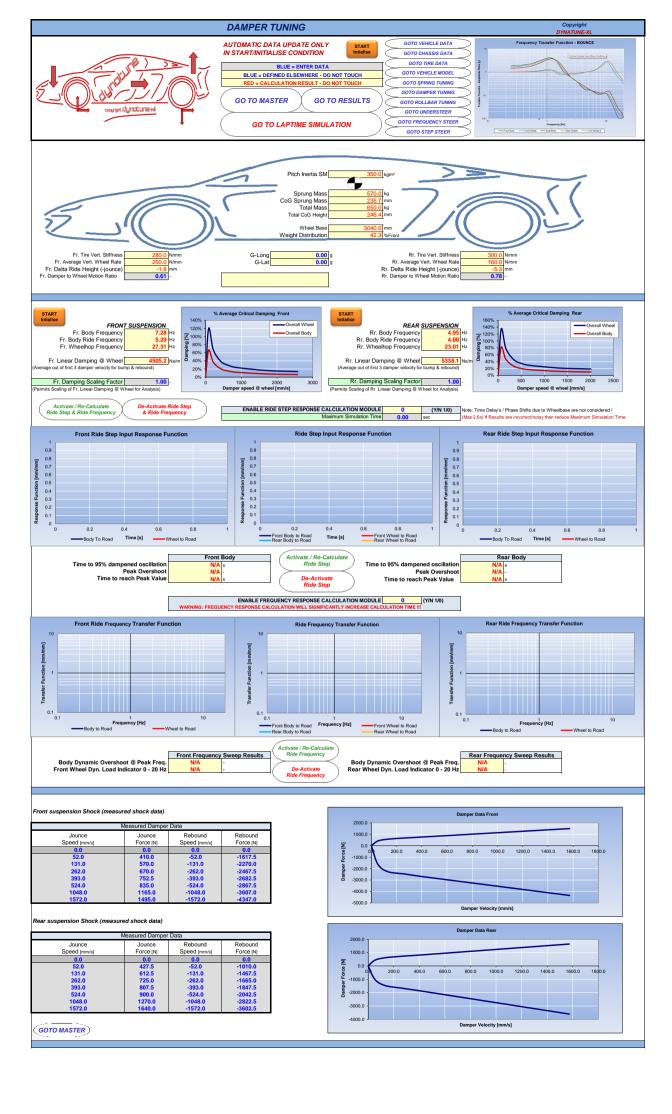
GEN	ERAL VEHICLE RE	FERENCE DATA						
	VELOCITY [kph]							
Front End	62.1	124.0	186.3	249.5	313.5			
Instant. Fr. Vertical Wheel Rate [N/mm]	250.0	250.0	250.0	900.0	1400.0			
Instant. Fr. Lateral Load Transfer Distribution [%]	45.8	45.4	46.0	64.6	64.9			
Instant. Fr. Average Tire Loaded Radius [mm]	327.4	327.0	325.7	323.7	321.2			
Instant. Fr. Ride Height Change (- = Jounce) [mm]	0.0	-1.9	-5.8	-9.6	-13.1			
Instant. Fr. Roll Center Height [mm]	-12.8	-15.4	-19.9	-24.5	-28.7			
Instant. Total Fr. Aerodynamic Lift [N]	-198.3	-812.9	-1917.0	-3464.2	-5231.6			
lody								
Instant. Total Drag Force [N]	-223.6	-887.1	-1976.0	-3487.8	-5446.5			
Instant. CoG Height SM [mm]	239.1	235.4	228.4	218.9	208.2			
Instant. Total CoG Height [mm]	249.8	246.1	239.2	229.7	219.1			
lear End								
Instant. Rr. Vertical Wheel Rate [N/mm]	160.0	160.0	160.0	160.0	320.0			
Instant. Rr. Lateral Load Transfer Distribution [%]	54.2	54.6	54.0	35.4	35.1			
Instant. Rr. Average Tire Loaded Radius [mm]	326.1	324.9	322.3	318.2	313.2			
Instant. Rr. Ride Height Change (- = Jounce) [mm]	-0.7	-5.7	-14.9	-28.6	-44.4			
Instant. Rr. Roll Center Height [mm]	80.6	74.9	64.9	50.5	34.1			
Inst. Total Rr. Aerodyn. Lift [N]	-369.9	-1512.1	-3521.4	-6402.4	-9796.5			











Output Parameter

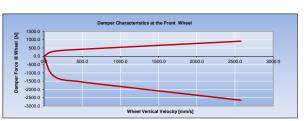
Calculated Front Damper Data @ WHEEL						
(C	onsidering motion	ratio)				
Jounce	Jounce	Rebound	Rebound			
Speed [mm/s]	Force [N]	Speed [mm/s]	Force [N]			
0.0	0.0	0.0	0.0			
85.2	250.1	-85.2	-986.7			
214.8	347.7	-214.8	-1384.7			
429.5	408.7	-429.5	-1505.2			
644.3	459.0	-644.3	-1636.3			
859.0	509.4	-859.0	-1749.2			
1718.0	710.7	-1718.0	-2200.3			
2577.0	912.0	-2577.0	-2651.7			

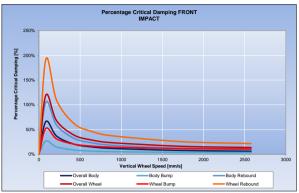
Front Body Percent Critical Damping for "IMPACT" events (damper "rate" from 0 to operating point)						
Wheel Vertical Speed [mm/s]	Overall Body	Body Bump	Body Rebound			
0.0	0.0	0.0	0.0			
85.2	0.66	0.27	1.06			
214.8	0.37	0.15	0.59			
429.5	0.20	0.09	0.32			
644.3	0.15	0.07	0.23			
859.0	0.12	0.05	0.19			
1718.0	0.08	0.04	0.12			
2577.0	0.06	0.03	0.09			

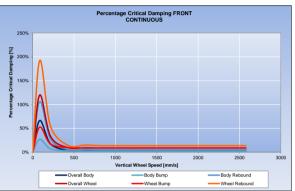
Front Wheel Percent Critical Damping for "IMPACT" events (damper "rate" from 0 to operating point)						
Wheel Vertical Speed [mm/s]	Overall Wheel	Wheel Bump	Wheel Rebound			
0.0	0.0	0.0	0.0			
85.2	1.20	0.52	1.92			
214.8	0.68	0.31	1.09			
429.5	0.39	0.20	0.62			
644.3	0.29	0.17	0.46			
859.0	0.24	0.15	0.38			
1718.0	0.16	0.12	0.26			
2577.0	0.14	0.11	0.22			

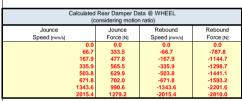
Front Body Percent Critical Damping for "CONTINUOUS" EVENTS (instantaneous damper rate)						
Wheel Vertical Speed [mm/s]	Overall Body	Body Bump	Body Rebound			
0.0	0.0	0.0	0.0			
85.2	0.66	0.27	1.06			
214.8	0.18	0.07	0.28			
429.5	0.04	0.03	0.05			
644.3	0.04	0.02	0.06			
859.0	0.03	0.02	0.05			
1718.0	0.03	0.02	0.05			
2577.0	0.03	0.02	0.05			

Front Wheel Percent Critical Damping for "CONTINUOUS" EVENTS (instantaneous damper rate)						
Wheel Vertical Speed [mm/s] Overall Wheel Wheel Bump Wheel Rebo						
0.0	0.0	0.0	0.0			
85.2	1.20	0.52	1.92			
214.8	0.33	0.17	0.55			
429.5	0.09	0.10	0.14			
644.3	0.09	0.09	0.15			
859.0	0.09	0.09	0.14			
1718.0	0.09	0.09	0.14			
2577.0	0.00	0.00	0.14			







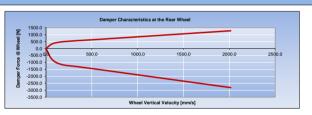


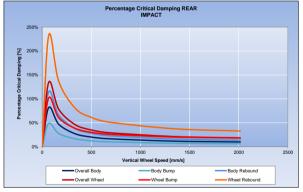
Rear Body Percent Critical Damping for "IMPACT" events (damper "rate" from 0 to operating point)						
Wheel Vertical Speed [mm/s]	Overall Body	Body Bump	Body Rebound			
0.0	0.0	0.0	0.0			
66.7	0.82	0.49	1.15			
167.9	0.47	0.28	0.66			
335.9	0.27	0.16	0.38			
503.8	0.20	0.12	0.28			
671.8	0.17	0.10	0.23			
1343.6	0.12	0.07	0.16			
2015.4	0.10	0.06	0.14			

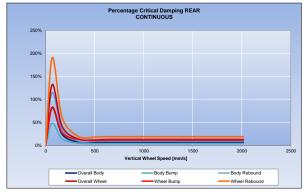
Rear Wheel Percent Critical Damping for "IMPACT" events (damper "rate" from 0 to operating point)					
Wheel Vertical Speed [mm/s]	Overall Wheel	Wheel Bump	Wheel Rebound		
0.0	0.0	0.0	0.0		
66.7	1.35	1.02	2.33		
167.9	0.78	0.61	1.37		
335.9	0.46	0.38	0.80		
503.8	0.35	0.30	0.61		
671.8	0.29	0.26	0.51		
1343.6	0.21	0.20	0.37		
2015.4	0.18	0.18	0.33		

Rear Body Percent Critical Damping for "CONTINUOUS" EVENTS (instantaneous damper rate)					
Wheel Vertical Speed [mm/s]	Overall Body	Body Bump	Body Rebound		
0.0	0.0	0.0	0.0		
66.7	0.82	0.49	1.15		
167.9	0.24	0.14	0.34		
335.9	0.07	0.05	0.09		
503.8	0.06	0.04	0.08		
671.8	0.06	0.04	0.09		
1343.6	0.06	0.04	0.09		
2015.4	0.06	0.04	0.00		

Rear Wheel					
Percent Critical Damping for "CONTINUOUS" EVENTS (instantaneous damper rate)					
Wheel Vertical Speed [mm/s]	Overall Wheel	Wheel Bump	Wheel Rebound		
0.0	0.0	0.0	0.0		
66.7	1.32	0.83	1.91		
167.9	0.41	0.27	0.60		
335.9	0.14	0.13	0.19		
503.8	0.12	0.11	0.18		
671.8	0.13	0.12	0.19		
1343.6	0.13	0.12	0.19		
2015.4	0.13	0.12	0.19		







motion ratio from 0 to 1 (1 = wheel travel)
* Unsprung mass is considered for each corner
** Damping in tire empirically considered (5% critical)
*** Bump positive, rebound negative

